


# STORMWATER MANAGEMENT PLAN

## FOR


# BELFAST WATER TREATMENT PLANT BANKABLE FEASIBILITY STUDY

# EXXARO




### COMPILED BY:

NAME	TITLE	SIGNATURE	DATE
Biermann du Plessis	Civil/Structural Engineer, PROXA		24.01.2025

### REVIEWED BY:

NAME	TITLE	SIGNATURE	DATE
Floris Stemmet	Project Manager, PROXA		
Preneesh Thulsi	Civil/Structural Engineer, PROXA		24.01.2025

### APPROVED BY:

NAME	TITLE	SIGNATURE	DATE
Tendani Dau	Senior Civil Engineer, Exxaro		2025/02/04
Rudolph Steenkamp	Project Engineering Manager, Exxaro		2025/01/31
Daan Killian	Project Manager, Exxaro		2025-01-31

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## TERMS, ACRONYMS AND ABBREVIATIONS

Table 1 lists the acronyms and abbreviations used in this document.

**Table 1: List of Acronyms and Abbreviations**

ABBREVIATION	DEFINITION
EIA	Environmental Impact Assessment
EXX	Exxaro
IWUL	Integrated Water Use License
NGL	Natural Ground Level
PCD	Pollution Control Dam
RFW	Raw Feed Water
WTP	Water Treatment Plant

## DEFINITIONS

The definitions listed below apply to this document. For more details, please consult the Glossary.

TERM	DEFINITION
ATTENUATION STRUCTURES	Infrastructure designed to temporarily store stormwater to reduce peak flows and allow for controlled release. This helps to prevent flooding and erosion downstream.
CLIENT	Exxaro.
CONTAMINATED STORMWATER	Stormwater that has come into contact with contaminants such as oil, chemicals, or heavy metals, typically from industrial or mining operations. This water may pose environmental risks and must be managed to prevent pollution.
EIA	A process used to assess the environmental and socio-economic impacts of a proposed project or development. In this context, the EIA evaluates the potential impacts of the proposed Water Treatment Plant facility at Exxaro Belfast Coal Mine.

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<b>TERM</b>	<b>DEFINITION</b>
ECSA	Engineering Council of South Africa.
ENERGY DISSIPATER	A structure or technique used to reduce the velocity of stormwater flow and prevent erosion or damage at the outlet of a drainage system. Common examples include rock rip-rap, gabions, and other engineered solutions.
ENGINEER	The individual, or company, responsible for the design, for preparation of the Drawings (or approval of Drawings prepared by others) and where applicable, inspection of construction for conformity with design.
FLOOD RECURRENCE INTERVAL	The frequency with which a given flood event (with a specified magnitude) is expected to occur, typically expressed as a ratio (e.g., 1:50-year or 1:20-year). A 1:50-year flood event has a 2% chance of occurring in any given year.
INTERLOCKS	Mechanical or electronic devices that ensure that certain systems (such as bunding and spill containment) operate in a controlled and safe manner, often used in chemical handling areas to prevent accidental spills or releases.
PCD	A facility used in industrial and mining settings to contain and manage contaminated water and prevent it from polluting the surrounding environment. PCDs are designed to store contaminated runoff until it can be treated or safely disposed of.
PRECIPITATION CATCHMENT AREA	A defined area that collects rainfall or other forms of precipitation, which then contribute to runoff that is directed through stormwater systems. This area's characteristics influence runoff calculations.
RUNOFF COEFFICIENT	A dimensionless value that represents the fraction of rainfall that becomes runoff from a particular surface. It is used to calculate stormwater runoff and varies depending on land use, surface type, and soil characteristics.
IWUL	A legal document issued by the Department of Water and Sanitation (DWS) in South Africa. It permits the holder (in this case, Exxaro) to use water for specific purposes, such as water treatment, discharge, or storage, while complying with environmental regulations.
SANRAL	South African National Roads Agency Limited.
SANS	South African National Standards.
SOILSAVER	A geotextile material used to stabilize soil on slopes or embankments, reducing erosion and promoting vegetation growth. It is commonly used in areas that require fast stabilization, especially in construction zones.
STORMWATER	Water that results from precipitation and runs off from land surfaces such as roads, buildings, and other hard surfaces. It is usually directed to stormwater drains and may require treatment or attenuation before discharge.
TIME OF CONCENTRATION	The time it takes for water to flow from the furthest point of a catchment area to the outlet. It is used to calculate peak flow rates in stormwater drainage systems and is influenced by factors such as catchment shape and slope.
V-DRAIN	A type of stormwater drainage channel with a V-shaped cross-section, often used in areas with significant surface runoff. V-drains are designed to direct water away from infrastructure while preventing erosion and flooding.
WTP	A facility designed to treat water (in this case, stormwater, contaminated water, or process water) to meet required quality standards before being released into the environment or used within the mining operation.

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## REFERENCES

The following documents are either **Applicable Documents** - applicable to the extent specified herein and thus forming part of this document. The applicability will generally relate to the Project in terms of policy, procedures, standards, qualification, etc.; or **Reference Documents** - where the information concerned has been fully extracted from the reference document and added to this document, or where the reference document contains information relevant to this document, or for information only.

NO.	DOCUMENT NAME	ACONEX DOCUMENT NUMBER
1	Design Requirements Storm Water Rev 1	EXX-ECL-STD-0011
2	Drainage Manual: The South African National Roads Agency Limited (5 <sup>th</sup> Ed.)	SANRAL Drainage Manual
3	Regulations on use of water for mining and related activities aimed at protection of water sources	NATIONAL WATER ACT, 1998 (ACT NO.36 of 1998)
4	WTP Area Block Plan	BCU-S01-730-ME-LO-0001
5	WTP Stormwater Layout and Management Plan	BCU-S01-729-CL-LO-0003
6	WTP Stormwater Details	BCU-S01-729-CL-DE-0001
7	Civil and Structural Design Criteria	BCX-000017-12955-ENG-DCR-0004
8	Civil and Structural Design Report	BCX-000017-12955-ENG-RPT-0022
9	Civil Design Requirements For Road Geometry	EXX-ECL-STD-0008

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## 1. INTRODUCTION/BACKGROUND

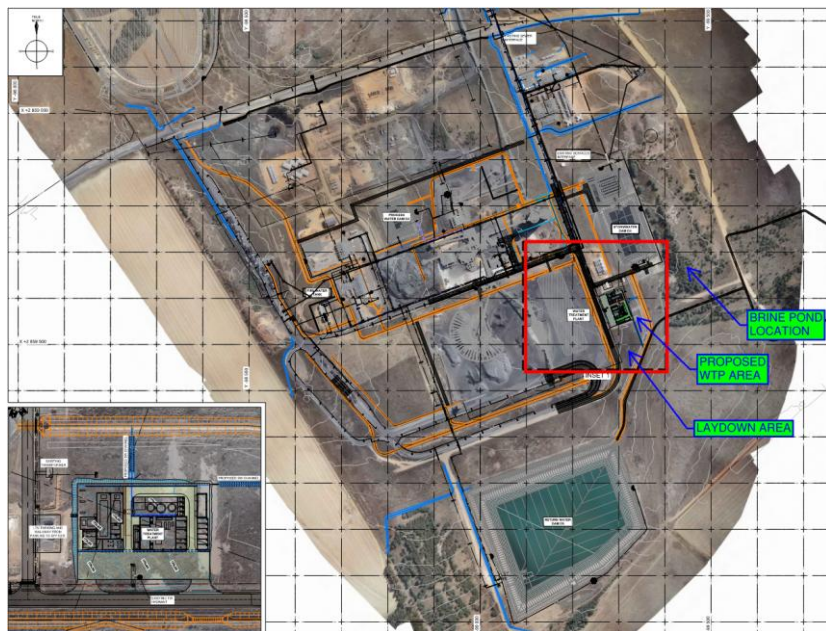
Exxaro Belfast Mine is exploring efficient and sustainable technological solutions to meet its current and future water treatment needs. This initiative is aimed at supporting the mine’s operational objectives while minimizing environmental impact. As part of this effort, multiple studies have been conducted to evaluate alternative water treatment technologies and processes, with the goal of improving water quality management on-site.

This report presents an assessment of the stormwater and contaminated stormwater systems required for the proposed Water Treatment Plant (WTP) facility infrastructure. The analysis focuses on the stormwater infrastructure on and around the newly proposed terrace, and outlines the solutions implemented to address runoff, contamination, and erosion, ensuring compliance with both Environmental Impact Assessment (EIA) and Integrated Water Use License (IWUL) requirements. The report provides detailed analyses of the stormwater and wash water management systems, including separate management approaches for stormwater and contaminated wash water.

## 2. PROJECT LOCATION

The proposed WTP facility will be located within the secured area of Exxaro Belfast Coal Mine, situated in the Mpumalanga Province, approximately 55 km east of Middelburg and 20 km south-west of Belfast. The site forms part of the Witbank Coalfield, situated to the south of the N4 highway.

The facility will be positioned to the south-east of the main plant and to the east of the existing export stockpiles, near PCD 4 (Pollution Control Dam 4), as depicted in the project layout plan below. The proposed facility will be integrated into an existing operational environment, where the design of the stormwater management system will ensure minimal disruption to the natural hydrology of the area.



**Figure 1: Proposed Site Layout**

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### **3. PURPOSE OF THE STORMWATER MANAGEMENT PLAN**

The primary purpose of the Stormwater Management Plan is:

- Safeguard the development and infrastructure of the WTP.
- Preserve the surrounding natural environment and water resources.
- Protect existing streams, wetlands, and drainage lines wherever feasible.
- Mitigate the anticipated increase in surface runoff into natural drainage systems.
- Maintain water quality by protecting underground resources from contamination.
- Protect existing on-site infrastructure services.
- Implement efficient methods to control and manage runoff.
- Pursue environmental sustainability in parallel with economic development goals.

The Wash Water Management Plan specifically aims to:

- Protect the development, mine property, and infrastructure.
- Facilitate drainage around critical infrastructure.
- Contain and manage potentially contaminated water to prevent contamination of the natural environment.

## **4. DESIGN PHILOSOPHY AND PROPOSED STORMWATER SYSTEM**

### **4.1 OVERVIEW**

The stormwater management system will be designed to minimize disruption to natural drainage systems. Efforts will be made to collect and manage stormwater in designated areas and release it in an environmentally responsible manner, while preserving and protecting natural drainage routes where possible. Dirty water will be contained and/or discharged into the mine's existing dirty water stormwater systems.

### **4.2 EROSION CONTROL AND SURFACE RUN-OFF MANAGEMENT**

Design measures will incorporate erosion protection at key stormwater outlets. This is essential due to the higher concentrated flow velocities from drainage channels, such as V-drains. Erosion control solutions will include the use of stone pitching, energy dissipators and lined drains.

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To further reduce erosion risks, the following additional measures will be implemented:

- The establishment of more frequent cut-off channels and berms to redirect overland flow from hardstand areas.

It is imperative that the stormwater system remains separate from contaminated water systems. All wash water inside bunded areas will be collected in sumps within bunded areas, where it will be pumped back into the process plant for treatment, avoiding discharge into the environment.

### 4.3 ROADS AND HARDSTANDS

The design of internal roads will include crossfalls to direct runoff to the road edges, minimizing ponding. Stormwater will be collected via grated channels and concrete-lined v-drains, ultimately being conveyed to the main trapezoidal stormwater channel, which will discharge into the bulk stormwater collector located below the site and eventually release into Dam 5.

Hardstand areas, roads, and terraces will be considered "hardened" surfaces with a runoff coefficient that reflects their impervious nature. Natural, sandy areas will have a lower runoff coefficient due to their ability to absorb water, especially where vegetation is minimal.

### 4.4 STORMWATER HYDROLOGY AND METHOD OF ANALYSIS

The Rational Method will be employed for estimating peak stormwater runoff rates. This method is widely used for small to medium-sized catchments due to its simplicity and ease of application. While the Rational Method has some limitations, such as the assumption of uniform rainfall intensity and the need for expert judgment in selecting runoff coefficients, it remains suitable for estimating runoff in catchments smaller than 15 km<sup>2</sup> in South Africa.

The method will be applied using the following basic rainfall data for the region:

**Table 2: Rainfall Data**

Return Period	Rainfall Depth (mm)	Rainfall Intensity (mm/hr)
1:5	26	104
1:10	32	128.1
1:20	39.4	157.7
1:50	51.9	207.6

The Rational Method  $Q = \frac{f_t * C * A * I}{(1000 * 3600)}$ , where

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- Q = the maximum/peak rate of run-off in cubic metres per second (m<sup>3</sup>/s)
- f<sub>t</sub> = Adjustment factor for the recurrence interval storm considered
- C = Run-off coefficient
- I = Rainfall intensity (mm/hour)
- A = Catchment area (m<sup>2</sup>)

The design parameters for the storm water infrastructure to be installed for the mine can be summarised as follows:

- Flood recurrence intervals (Bulk Network) : 1:50
- Flood recurrence intervals (Internal Network) : 1:20
- Design life of Attenuation structures : 50 years
- V-drain Material : Concrete
- Concrete strength : 35 MPa
- Blinding : 10 MPa
- Bedding Material : Class C

#### 4.5 DRAINAGE SYSTEM DESIGN

Stormwater channels will be designed using established empirical formulas such as Manning's and Chezy's for open-channel flow. The hydraulic design will account for factors such as concrete roughness, flow transition losses, and bend losses. From flow calculations using the Mannings n-value, the absolute roughness k-value was calculated.

Design criteria for hydraulic analysis of drainage systems.

- Stormwater systems inside the plant are designed for 1:20 year peak flow (conservative approach).
- Open stormwater main collectors are designed as trapezoidal 600 mm minimum width with side slope of 1:2.
- All the channels in the dirty water area are concrete lined. Channels conveying clean water are either unlined unless the velocity criteria and minimum slope necessitates the channel to be lined.
- Permissible velocity in reinforced concrete lined channels is 6 m/s and joints should be design to withstand pulsating pressure changes for velocities higher than 2.5m/s. The linings of channels that carry high-velocity flow should be poured as nearly monolithic as possible, without expansion joints or weep holes, and using as few construction joints as possible. Construction joints

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should be made watertight. Longitudinal and transverse reinforcing steel should be used throughout to control cracking with the longitudinal steel carried through the construction joints. The lining should be anchored to the slope as necessary by reinforced cut-off walls to prevent sliding.

#### 4.6 TIME OF CONCENTRATION (TC)

The time of concentration is defined as the duration it takes for the excess rainfall, which results in runoff, to travel from the most distant significant point of a natural catchment to the designated point of interest. The shape of the catchment plays a crucial role in determining the length of the flow path.

Given that the catchments in the area are relatively small (< 1 km<sup>2</sup>), we recommend using a minimum time of concentration of 15 minutes for all undeveloped areas. This means that if the calculated time of concentration for an industrial site is less than 15 minutes, 15 minutes should be used instead :

- Storm event period – 15 minutes
- Time of Concentration - 15 minutes
- Retention time - 15 minutes
- MAP = 697 mm

#### 4.7 RUN-OFF COEFFICIENTS (C)

Allowances have been made for the various areas and their contribution to the flow and the coefficient of runoff for the various areas is as follows:

The runoff coefficient, denoted as "C," is a value between 0 and 1 that accounts for variations in rainfall across the catchment, infiltration, overland flow velocity during a storm, catchment shape, ground slope, and other factors. Due to numerous uncertain variables, such as soil moisture, vegetation, soil permeability, slope variations, and rainfall intensity, estimating the coefficient "C" can be challenging. As a result, there can be a wide range of possible runoff coefficients. To ensure consistency and minimize discrepancies, the Department of Water Affairs & Sanitation (DWS) table method will be used.

- Grassed areas are taken as 0.35
- Buildings and surfaced roads and hardstands are taken as 1.00
- Gravel roads, terraces, hardstand areas are taken as 0.9

The value of "C" can be obtained from relevant tables. If multiple catchments or sub-catchments contribute to the runoff at the point of interest, and if the values of "C" are not uniform (i.e., there are variations in slopes, vegetation, etc.), then a modified coefficient must be calculated using the following formula:

Overall = (Sum of Ci x Ai) / (Sum of Ai) for all differing sub-catchments "i".

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For undeveloped sites, the value for "C" is determined by summing the contributions of ground slope (Cs), vegetation cover (Cv), and soil permeability or type (Cp). In urban or industrial areas, it is appropriate to combine the percentage contribution of hardened areas with the remaining site area, which is assessed in terms of Cs, Cv, and Cp as described:

$$C_i \text{ for catchment "i"} = C_{si} + C_{vi} + C_{pi}$$

For smaller catchments (<5 km<sup>2</sup>), the value of "C" may be considered constant during a storm. However, we recommend applying a modification factor (ft) to reduce runoff for lower-order storms:

- 2 year – ft = 0.50
- 5 year – ft = 0.55
- 10 year – ft = 0.60
- 20 year – ft = 0.67
- 50 year – ft = 0.83
- 100 year – ft = 1

The project has one main area of development that influences the stormwater drainage system which can be split up between the entrance hardstand area, roofs and bunded areas and roads. All stormwater calculations are attached in the appendices.

#### 4.8 ROUGHNESS COEFFICIENTS

The design of drainage waterways, culverts and structures shall be based on sound hydraulic principals in order to effect an optimum combination of efficiency and economy. Roads and hardstands drainage channels shall be designed using the Manning formulae with coefficients of roughness shown in the table below.

**Table 3: Open Channel – Manning Roughness Coefficients:**

<b>Open Channel Manning Roughness Coefficients</b>	
<b>Lined channels</b>	
Concrete	0.014
Grouted stone	0.025
Rock Rip-Rap	0.035
Paving Blocks	0.025
Gabion	0.028
<b>Unlined channels</b>	
Earth uniform section	0.030
Rock cuts	0.040

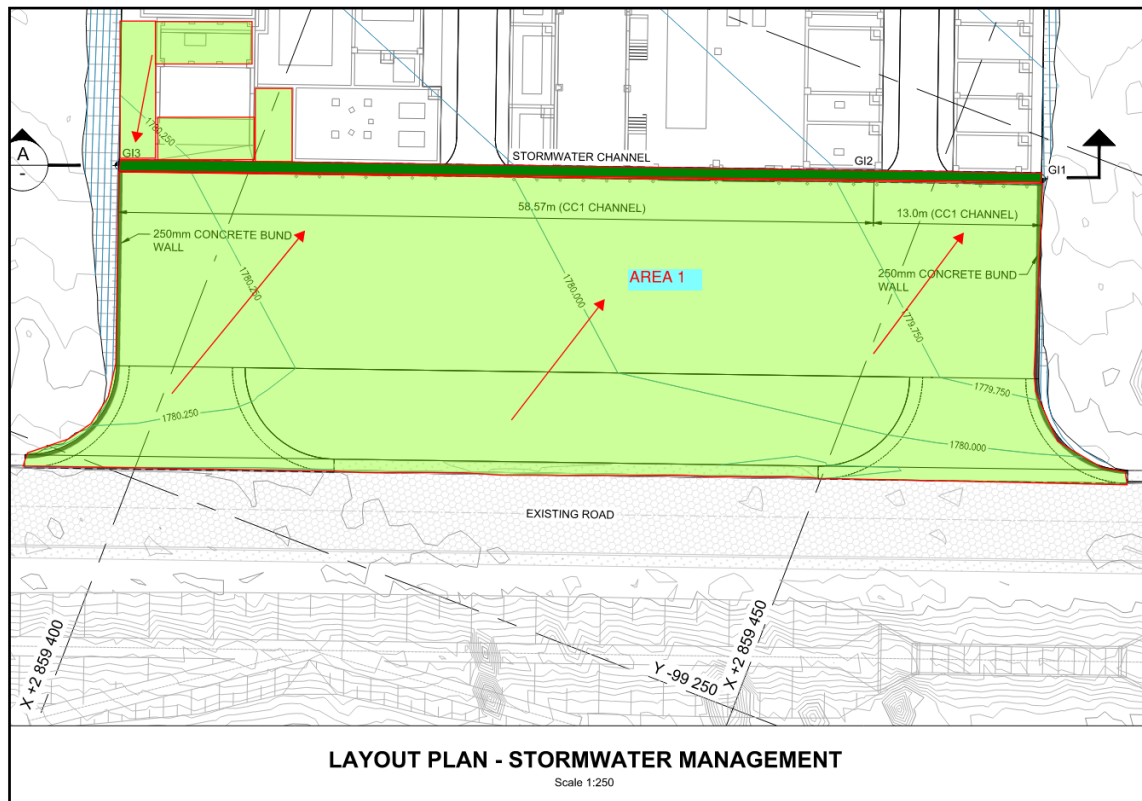
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## 5.2 ENTRANCE AREA 1

The entrance area is approximately 1850m<sup>2</sup> and slopes in a northerly direction. This area consists of a concrete hardstand, both entrance and exit bellmouth's and minimal roofed area. There is a centrally placed rectangular concrete channel that extends across the terrace to collect all the stormwater generated from the entrance area and hardstands between the water treatment plant and the existing road.

This concrete channel will include a sump measuring 500mm wide, 500mm deep, and 1000mm long, located near the process building to help pump contaminated water back into the water treatment plant. The channel and sump, with a total capacity of approximately 35m<sup>3</sup>, are designed to handle runoff from a 1:20 year storm in case the sump pump fails. Bund walls are installed at both ends of the channel to contain stormwater on the platform and prevent overflow onto the terrace slopes. In the event of a larger storm (with a non-functioning sump pump), any excess water will flow east along the road between the process plant and chemical store, where it will be captured by the "Area 3" dirty water concrete channel along the terrace edge, which directs water into the mine's dirty water system. The channel is equipped with a bund wall to ensure any overflows at GI 1 are redirected toward the road.



**Figure 3: Area 1 - Stormwater Bunded Channel**

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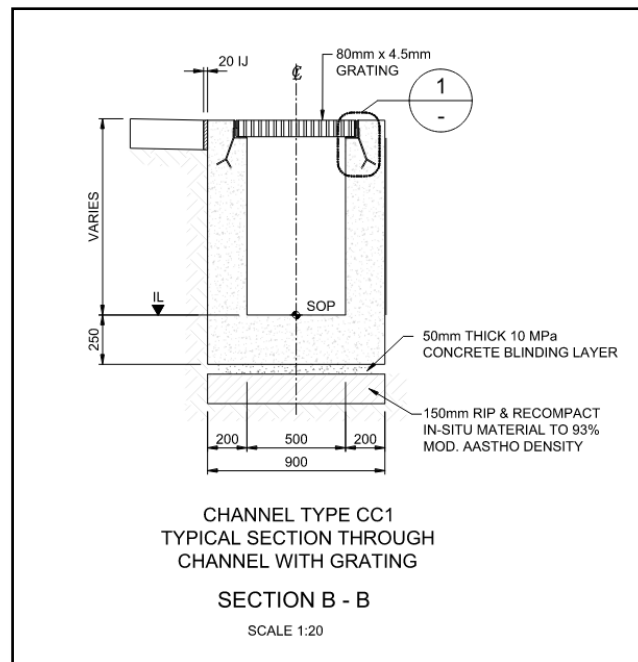
AREA 1			15 min minimum	15			
			1:20 years peak flow				
				Exxaro standards			
		Rainfall from Exxaro	157,7				
<b>RUN OFF CALCULATIONS</b>							
Surface Description	Unit	Amount	Area (m <sup>2</sup> )	C	Ft	A*C*Ft	Peak Flow (1:20) (m <sup>3</sup> /sec)
developed Land	m <sup>2</sup>	1850	1850,00	0,9	0,67	1115,55	0,049
<b>TOTAL</b>			<b>1850,00</b>			<b>Qri(pre)</b>	<b>0,049</b>

**Figure 4: Area 1 - Stormwater Calculations**

**5.3 MCC/CIP/RFW TANKS INTO CONCRETE CHANNEL AREA 2**

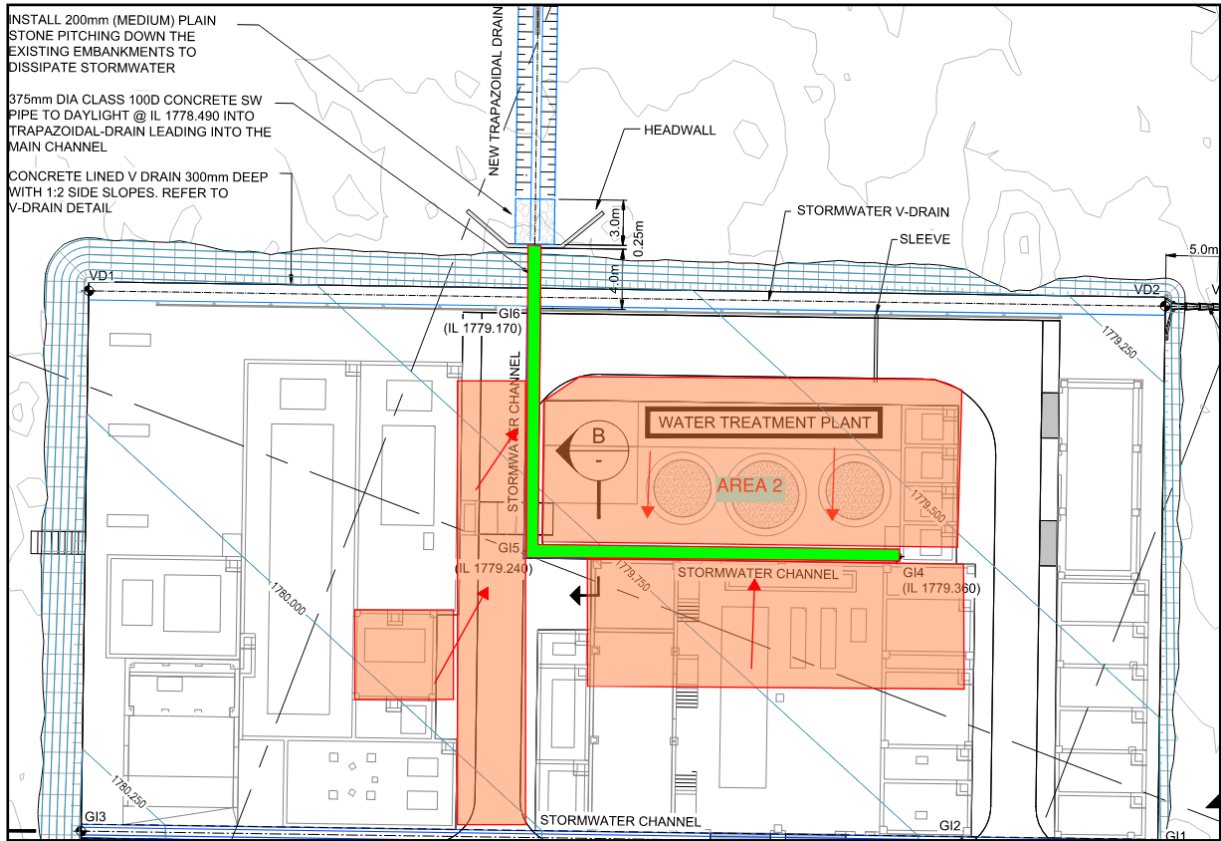
The area around the MCC/CIP/RFW tanks includes a concrete slab and pavers to manage spillage and wash water. The mentioned area drain towards the grated inlet depicted in Figure 5. The internal road network also contributes to this channel as a small section of road slopes towards the channel. The channel has a heavy duty grating specified to allow for heavy operating machinery to pass over the channel without compromising the structural integrity. Stormwater is conveyed through this channel towards the eastern side of the site into a 375mm diameter concrete Class 100D pipe to cross beneath the v-drain. Stormwater will release into a new lined trapezoidal collector off the terrace. Stormwater will be discharged into the main collector further east and will eventually release into dam 5.

NOTE: In the unlikely event that the incoming water to the RFW tanks overflow, the discharge will flow onto an apron slab directed towards the abovementioned concrete channel.



**Figure 5: Area 2 - Stormwater Concrete Channel Section**

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**Figure 6: Area 2 - Stormwater Concrete Channel**

AREA 2			15 min minimum	15			
			1:20 years peak flow				
			Rainfall from Exxaro	157,7	Exxaro standards		
<b>POST DEVELOPMENT RUN OFF CALCULATIONS</b>							
Surface Description	Unit	Amount	Area (m <sup>2</sup> )	C	Ft	A*C*Ft	Peak Flow (1:20) (m <sup>3</sup> /sec)
developed Land	m <sup>2</sup>	700	700,00	0,9	0,67	422,10	0,018
<b>TOTAL</b>			<b>700,00</b>			<b>Qri(pre)</b>	<b>0,018</b>

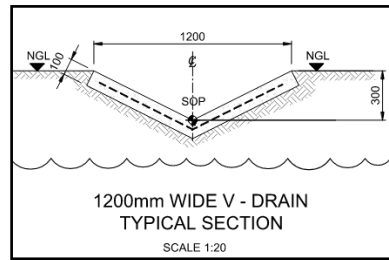
**Figure 7: Area 2 - Stormwater Calculations**

**5.4 V-DRAIN ON PLATFORM AREA 3**

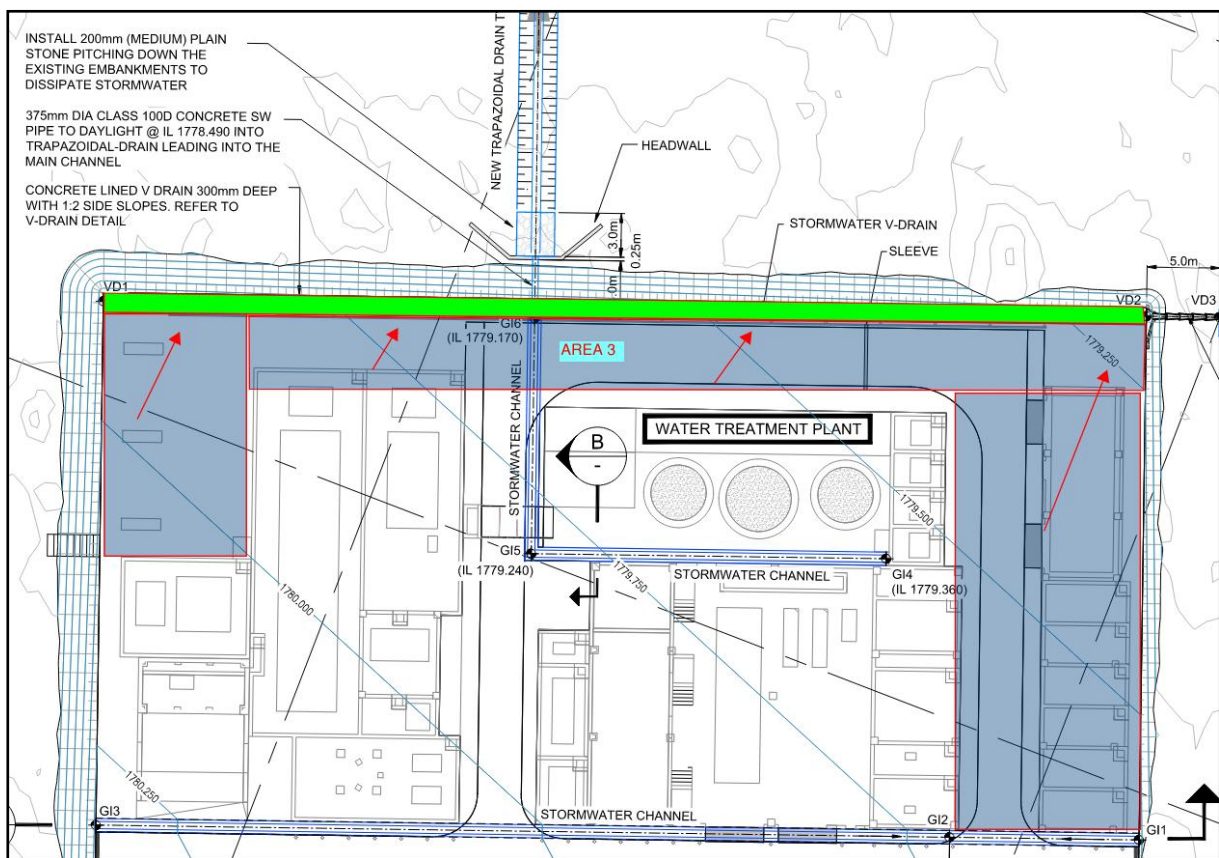
The v-drain on the eastern boundary of the terrace collects and conveys approximately 22% of all stormwater on terrace. The hardstand surface on site has a run-off factor “C” of 0.9 to determine peak flows within the concrete lined v-drain. This channel is located outside any trafficked areas with a Armco barrier installed along the length of the channel to provide protection against maintenance and operating equipment. The v-drain is 300mm deep with 1:2 side slopes which is sufficient to convey the amount of water that is generated from the mentioned area. Stormwater are being conveyed through this channel at a peak flow rate of 0.025m<sup>3</sup>/sec. Stormwater to be conveyed towards the southern side of the site into precast chutes to manage drainage down the terrace into a new lined trapezoidal collector.

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Stormwater will be discharged into the main collector further east and will eventually release into dam 5.



**Figure 8: Area 3 - Stormwater V-drain Section**



**Figure 9: Area 3 - Stormwater Concrete Channel**

AREA 3		15 min minimum	15				
		1:20 years peak flow		Exxaro standards			
		Rainfall from Exxaro	157,7				
<b>RUN OFF CALCULATIONS</b>							
Surface Description	Unit	Amount	Area (m <sup>2</sup> )	C	Ft	A*C <sup>2</sup> Ft	Peak Flow (1:20) (m <sup>3</sup> /sec)
developed Land	m <sup>2</sup>	950	950,00	0,9	0,67	572,85	0,025
<b>TOTAL</b>			<b>950,00</b>			<b>Qri(pre)</b>	<b>0,025</b>

**Figure 10: Area 3 - Stormwater Calculations**

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## 5.5 BUNDED AREAS ON PLATFORM AREA 4

The WTP includes several critical process areas that are designed with banded systems to manage hazardous materials. These bunds serve as secondary containment mechanisms to ensure the safe containment of any potential spills, leaks, or catastrophic failures within the respective facilities. The bunding design philosophy for each area has been specifically tailored to address the risk associated with the storage and handling of chemicals and other hazardous substances. The following outlines the banded areas, their respective capacities, and the design principles that guide their implementation:

**Table 4: Hazardous Chemical Storage Facilities**

<b>Banded Area</b>	<b>Bund Capacity Design Philosophy</b>
Chemical Store	Secondary containment for catastrophic failure. The bund is designed to contain at least 110% of the volume of the largest Intermediate Bulk Container (IBC), or 25% of the total volume of all IBPs, whichever is greater. Additionally, the Process Engineers will ensure that the chemicals stored in these containers are compatible with one another to prevent hazardous reactions in the event of a spill.
CIP Station (Cleaning-in-Place)	Secondary containment for catastrophic failure. The bund must have a capacity of at least 110% of the volume of the largest vessel within the bund. The design ensures containment in the event of an equipment failure or accidental spill.
Dosing station	Secondary containment for catastrophic failure. The bund is sized to contain at least 110% of the largest vessel stored within the station, ensuring containment in case of a spill or failure.
Lime Silo and Lime Mixing Tank	Secondary containment for occasional spillages and stormwater runoff. The bund must have a capacity of at least 25% of the total silo volume to capture potential spillages or runoff, particularly during storm events.
Coagulant	Secondary containment for catastrophic failure. The bund is designed to contain at least 110% of the largest container used for coagulant storage, ensuring that the area is protected from any spill or failure.
Backwash Clarifier	Secondary containment for occasional spillages and stormwater runoff. The bund is designed to hold at least 25% of the clarifier's volume, providing adequate containment for minor spills or run-off during wet weather conditions.
Gypsum Reactor and Clarifier	Secondary containment for occasional spillages and stormwater runoff. The bund capacity is designed to be at least 25% of the clarifier's volume or 10% of the reactor's volume, whichever is greater. This reflects the reduced risk associated with the reactor due to the presence of interlocks and automated control systems that minimize the potential for failure.
Sludge Tank	Secondary containment for occasional spillages and stormwater runoff. The bund is designed to contain at least 110% of the largest tank's volume, ensuring sufficient capacity to manage accidental releases or overflow events.

These banded areas are strategically designed to mitigate the risk of hazardous material release into the environment. They are sized based on the potential for either catastrophic failure or minor spills and runoff.

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The bunds have been carefully engineered to handle stormwater runoff and other incidental spillages during routine operations. Specifically, these bunds are capable of managing storm events with a 1:50-year return period, designed to withstand peak flows for a 15-minute duration without overtopping or causing environmental discharge.

These bunding systems are crucial for ensuring that hazardous materials remain safely contained within designated areas, reducing the risk of contamination or harm to the surrounding environment. The stormwater runoff captured by these bunds will be managed through appropriate drainage systems to prevent any unintended discharge of hazardous substances during heavy rain or other extreme weather events.

It should be noted that the bund capacity is calculated based on a flat surface. However, in reality, the surface is cast to the gradient off the terrace, and the height of the bund walls increases, which provides additional capacity. This extra volume will be considered as additional freeboard capacity.

**Table 5: Stormwater Bunded Area Calculations**

<b>Bunded Area</b>	<b>Bund Capacity (m<sup>3</sup>)</b>	<b>Required Capacity for Spillage (m<sup>3</sup>)</b>	<b>Required Capacity for SW (m<sup>3</sup>)</b>	<b>Worst Case % Utilised</b>
Dosing Station	1.76	1.65	0.19	93.75
Lime Silo	14.22	14.00	2.20	98.47
Coagulant	1.76	1.10	0.27	62.50
Backwash Clarifier	18.95	12.50	2.93	65.95
Gypsum Reactor	23.51	12.50	3.63	53.17
Sludge Tank	10.08	10.00	1.30	99.22

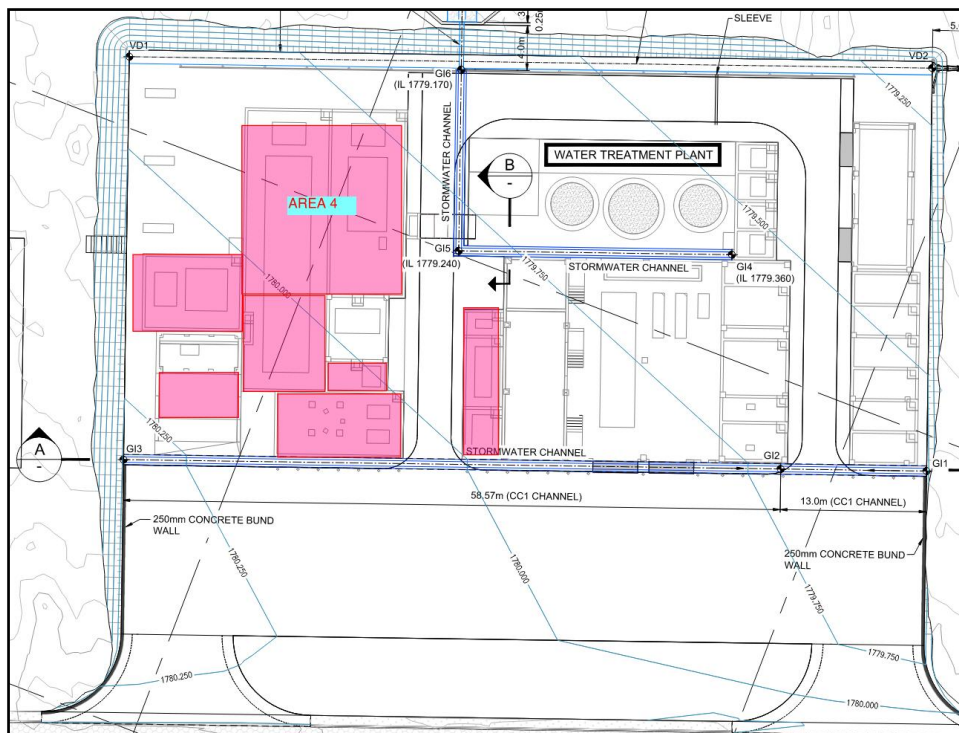
**NOTE:** The "Worst Case % Utilised" refers to the ratio of the bund's total capacity that is used in the worst case scenario, where either the hazardous material spillage and the stormwater runoff are taken into account.

The bund capacity calculations ensure that these areas will not only contain hazardous materials but also effectively manage stormwater runoff, minimizing the risk of contamination and environmental harm during adverse weather conditions. The above bunded areas were assessed as they are exposed to weather conditions and do not have a canopy or enclosure.

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RUN OFF CALCULATIONS									
Surface Description	Area (m <sup>2</sup> )	C	Ft	A*C*Ft	Peak Flow (1:10) (m <sup>3</sup> /sec)	Pre-Development Run Off Vri(pre)=Qri*60*Tc(m <sup>3</sup> )	Bund Capacity	Check	
Dosing Station	5,03	0,90	0,83	3,75	0,0002	0,19	1,76	OK	
Lime Silo	56,87	0,90	0,83	42,48	0,0024	2,20	14,22	OK	
Coagulant	7,04	0,90	0,83	5,26	0,0003	0,27	1,76	OK	
BW Clarifier	75,81	0,90	0,83	56,63	0,0033	2,93	18,95	OK	
Gypsum Reactor	94,03	0,90	0,83	70,24	0,0040	3,63	23,51	OK	
Sludge Tank	33,60	0,90	0,83	25,10	0,0014	1,30	10,08	OK	

**Figure 11: Area 3 - Stormwater Bunded Areas Calculations**



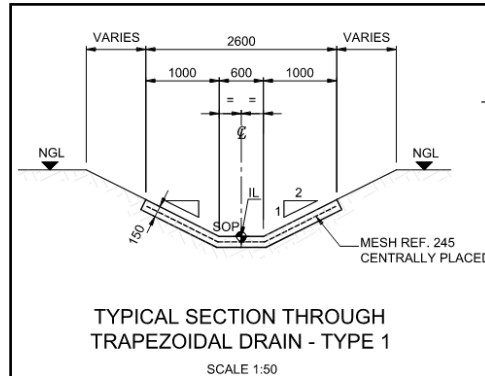
**Figure 12: Area 3 – Layout of Bunded Areas**

## 5.6 AREA SURROUNDING THE WTP TERRACE

The natural ground levels around the WTP terrace, between the gravel road and the existing dirty water channel from Dam 4 to Dam 5, slope generally from north-west to south-east. Therefore, stormwater will be collected in the new channels or the existing dirty water channel, as is currently the case. Although the runoff factor from the WTP terrace increases, the processing plant area does not contribute entirely to runoff, so there is minimal increase in overall runoff into Dam D5 compared to current conditions. The only areas on the platform that will additionally contribute in run-off is Area 2 and Area 3 which generates an additional 34m<sup>3</sup> of stormwater during a 1:50 year 15 minute storm intensity which is negligibly small. However stormwater is still

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being released in a controlled manner and mitigation measures are in place to control erosion.



**Figure 13: Stormwater Main collector off the platform**

## 6. MONITORING AND MAINTENANCE

### 6.1 MONITORING

The storm water system must be monitored during construction at regular intervals by the Environmental Control Officer (ECO) in terms of the Environmental Management Programme (EMPr).

During the construction phase of the development, the construction process should be monitored against the EMPr, and should pay attention to the following aspects:

- Implementing temporary attenuation measures, such as earth berms to retain surface run-off from construction activities and to avoid any damage to construction works.
- Providing a silt screen at all grid inlets to collect debris and silt during times of heavy rain.
- Controlling dust, especially during the construction of roads and platforms.
- Placing topsoil and grass sods onto cut/fill embankments to reduce runoff and velocity, including the use of Soilsaver where embankments are steep.

On completion of the construction, the maintenance team will be responsible to monitor the storm water system and attenuation facilities to identify improvements / maintenance. The factors to be monitored include the functionality and impact of the system on platforms and open areas further downstream.

The post development monitoring process should be done at regular intervals (suggested 6 monthly) to include the following activities:

- Product (open grass lined drains, grid inlets, splay inlets, headwalls, concrete pipes, overflow/outlet structure).
- Type of maintenance (rehabilitation, improvement, new).

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- Urgency (immediate, next 6 months, next 12 months) and description of work to be carried out.

## 6.2 OPERATION AND MAINTENANCE

The stormwater system, as designed, requires no manual operation and is self-regulating. The sumps will be provided with submersible pumps specified by Proxa. Sumps are equipped with submersible pumps operated by plant staff. Routine inspections are conducted twice daily to ensure sump conditions are optimal and to check for any spillages (e.g., chemicals or sludge). Any spillages are cleaned and directed into appropriate sumps for recovery. Specific procedures are in place for sumps, such as the centrifuge building sump, which pumps sludge back into the sludge tank, and the process building sump, which normally directs water to the rainwater drain, with rerouting measures available in case of spills.

Preventative maintenance is carried out according to the manufacturer's recommended intervals, focusing on sump pumps and related equipment. This ensures the system operates efficiently and is maintained to its original design. Maintenance activities also prioritise addressing any potential issues promptly to prevent damage or failure.

During the construction phase, surface runoff will be carefully managed with temporary measures until the system is fully operational. The Environmental Control Officer (ECO) will oversee runoff monitoring during this period. Routine maintenance tasks include clearing drains, removing silt from collection points, controlling vegetation, and mowing embankments. For more specialised work, such as replacing stormwater pipes or addressing attenuation areas, it is recommended to engage specialist service providers.

Routine maintenance will be the responsibility of the maintenance team and should include:

- Clearing of side drains, storm water pipes and collection points.
- Removal of silt from collection points and silt traps.
- Plant/weed control.
- Cutting grass on embankments.

## 7. RECOMMENDATIONS

The following recommendations are made for the proposed Water Treatment Plant at Exxaro Coal Mine:

1. That the storm water design parameters used in the design of the storm water management system are accepted and approved.
2. The detail design of the storm water system includes recommendations of this plan.
3. The storm water system must be kept separate from the sewerage system.

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4. All chemicals, cement, fuel and other hazardous material used during construction should be stored in controlled areas.
5. Concentration of storm water should be prevented where possible, but energy dissipaters should be provided in areas of concentration.
6. On completion of the construction of hardstands, structures, roads and parking areas, all remaining exposed embankments and open areas must be vegetated as soon as possible, including the use of "Soilsaver", where necessary.
7. During the construction phase, the following aspects should be closely monitored by the ECO to ensure the contractor complies:
  - Temporary berms and cut-off drains must be provided on site to collect run-off, especially until the stormwater network are complete and functional.
  - Silt screens must be provided at the grid inlets / splayed construction during road construction.
  - Topsoil must be conserved on site and prevented from entering the stormwater system.
  - Exposed embankments, cut/fill slopes and open areas must be vegetated as soon as possible to reduce runoff.
  - Dust control during construction must be applied at all times.
  - Excess spoil material from topsoil or bulk earthworks must be placed in areas or even removed entirely off site to minimise silt deposition, scouring and soil erosion.
  - Post construction, all exposed areas must be covered in vegetation, grass or landscaped.

## 8. CONCLUSION

The stormwater management plan for the proposed WTP facility at Exxaro Belfast Mine has been designed to meet environmental and regulatory standards, ensuring the protection of local water resources and the surrounding environment. The proposed system offers a comprehensive solution to manage both clean and contaminated stormwater, while promoting sustainable development and mitigating potential environmental impacts.

By integrating sustainable stormwater management practices and ensuring compliance with EIA and IWUL guidelines, the project aims to improve operational efficiency while minimizing the mine's environmental footprint.

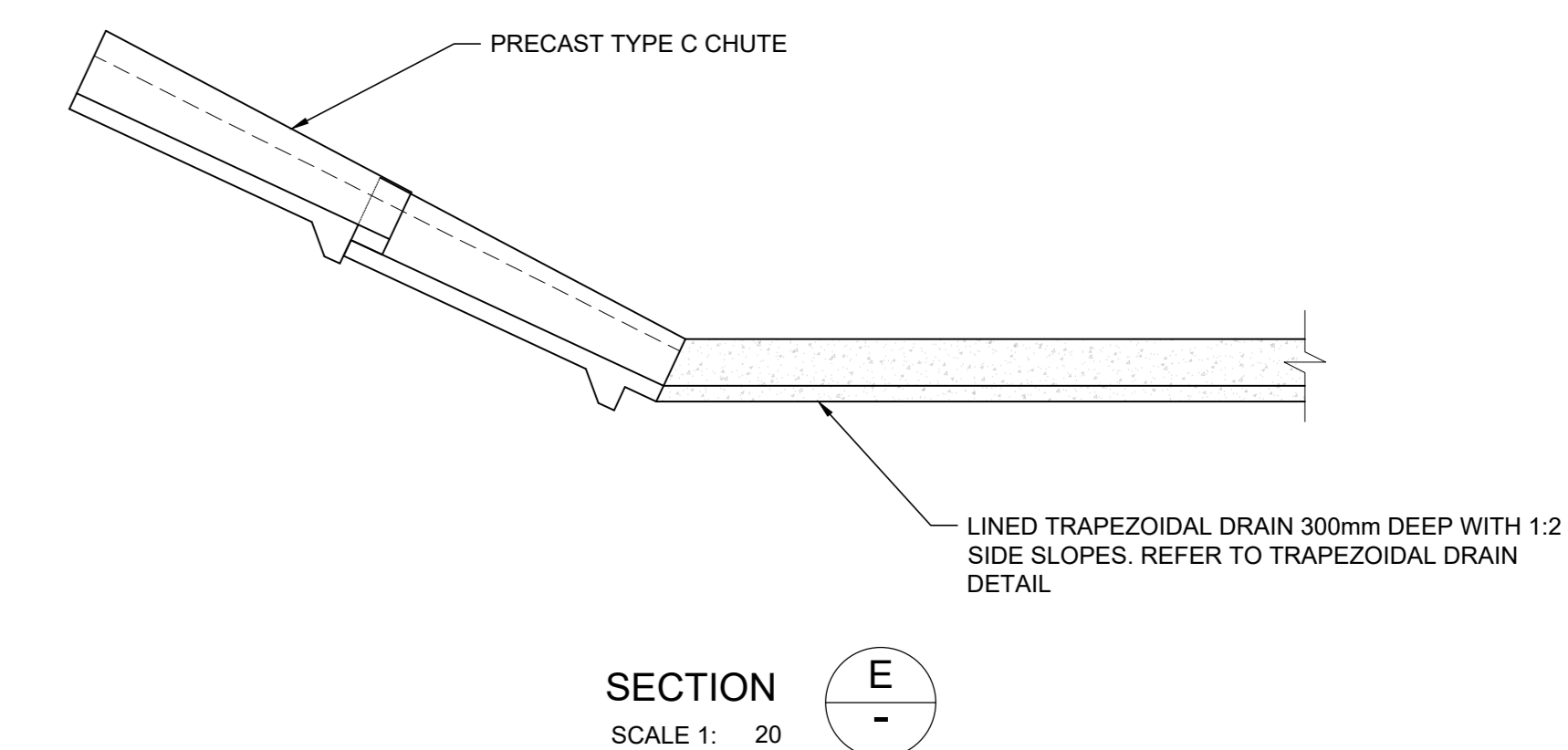
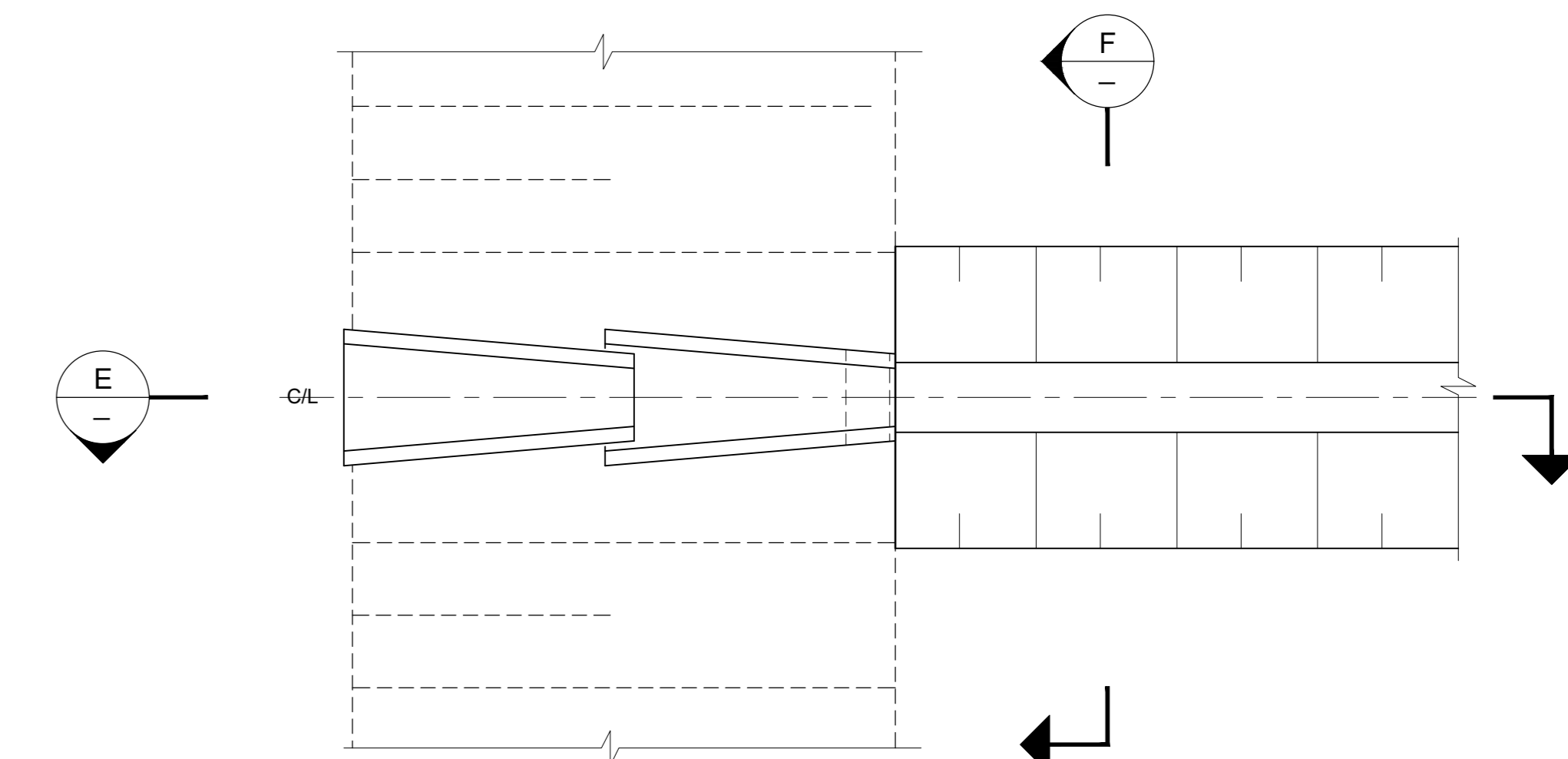
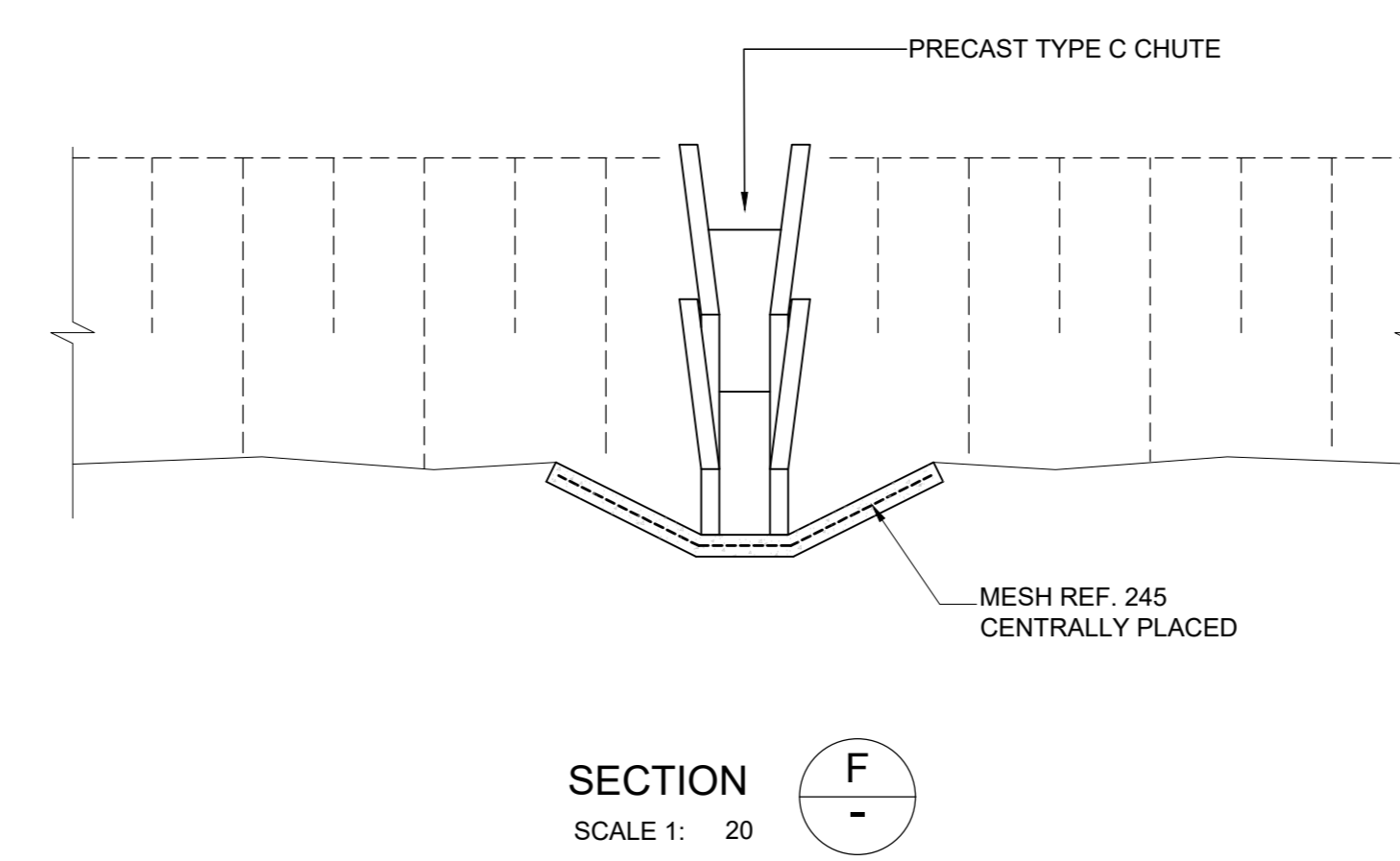
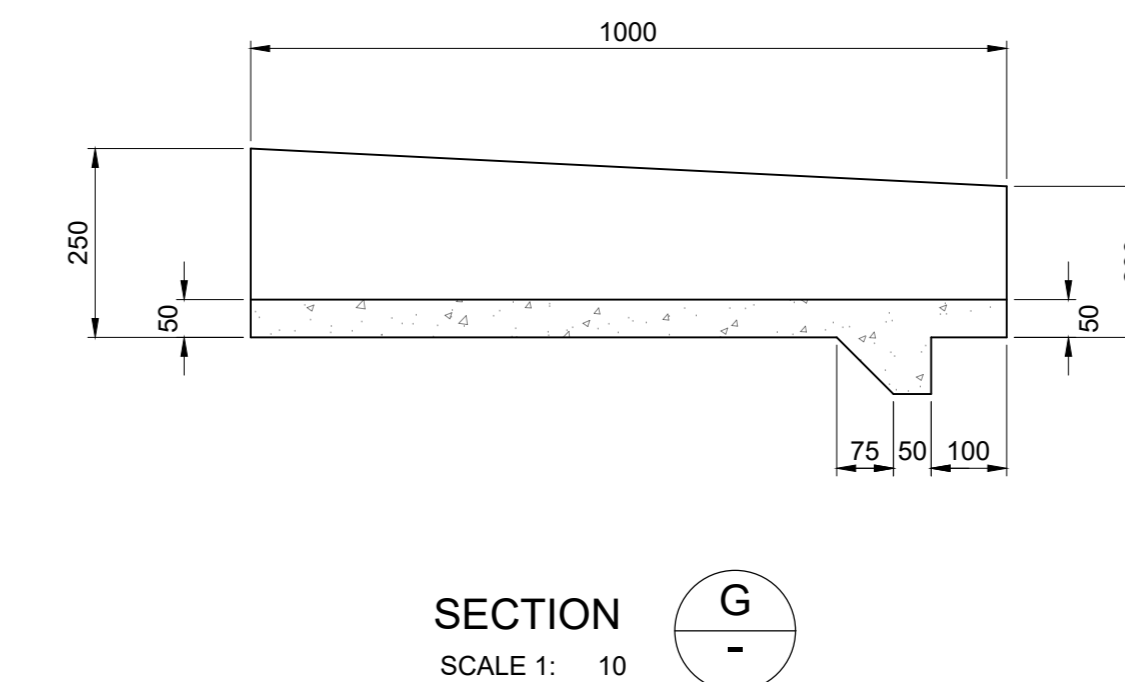
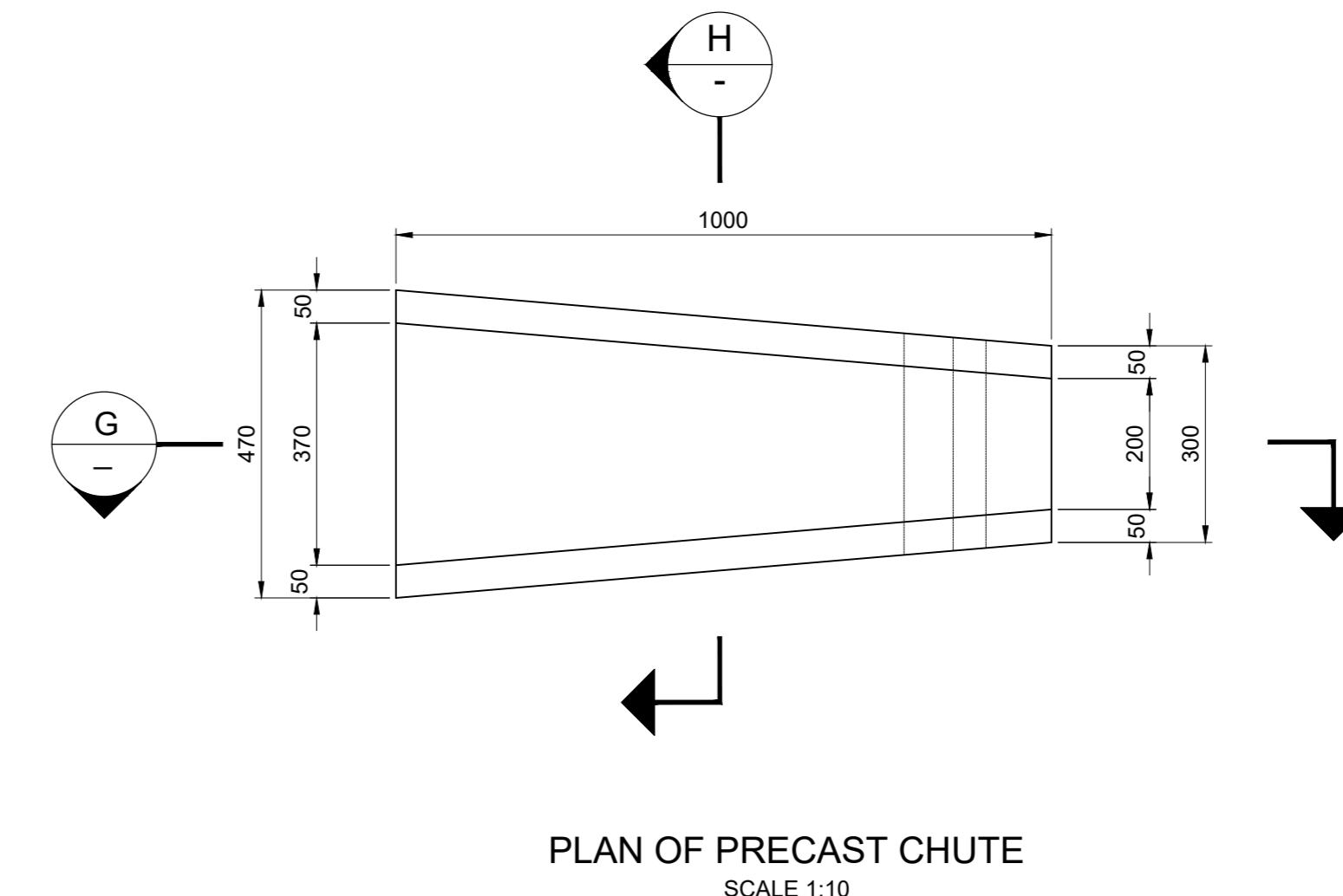
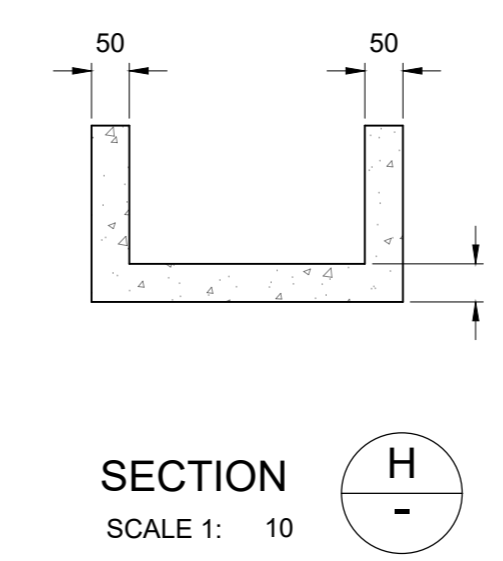
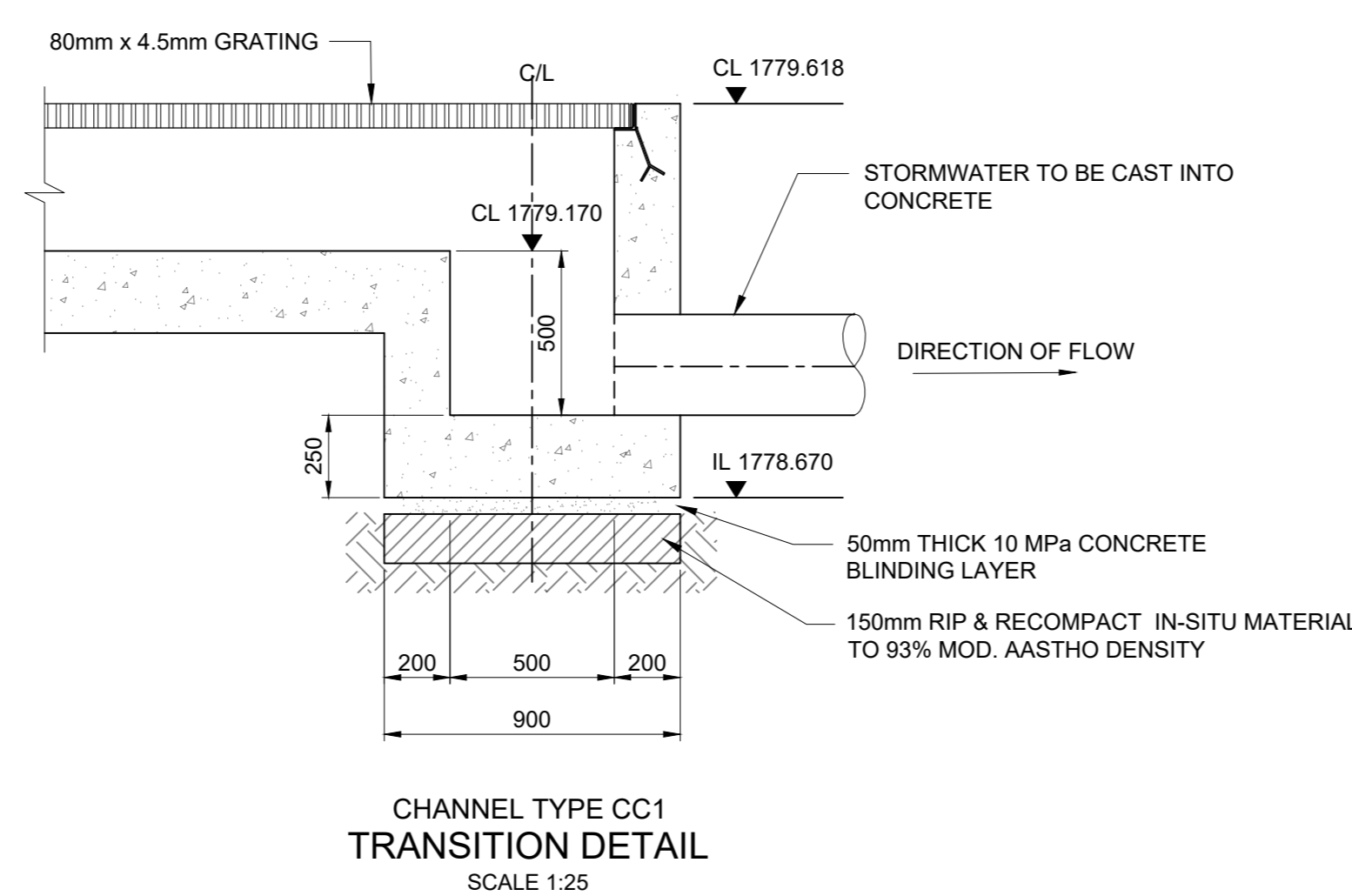
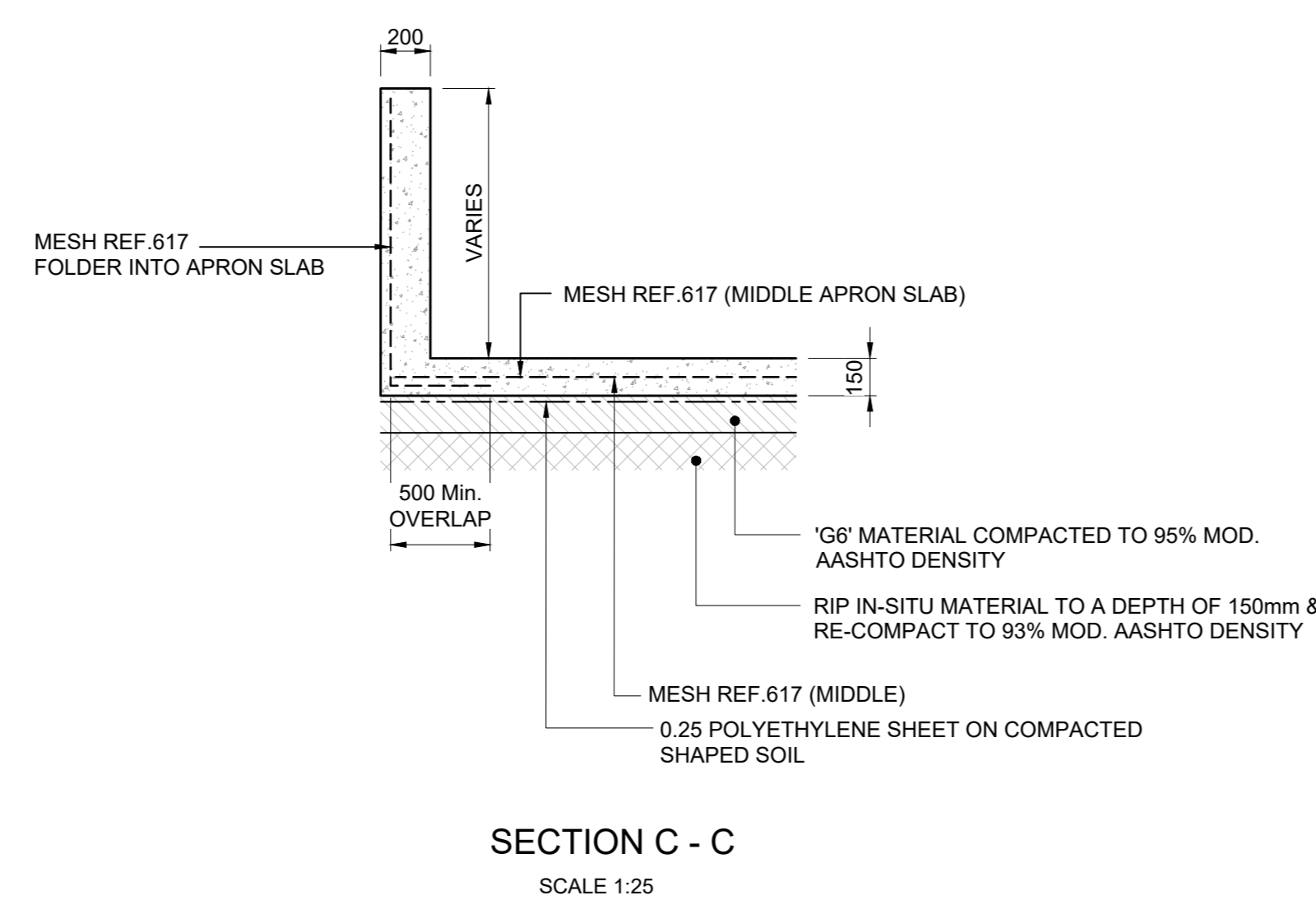
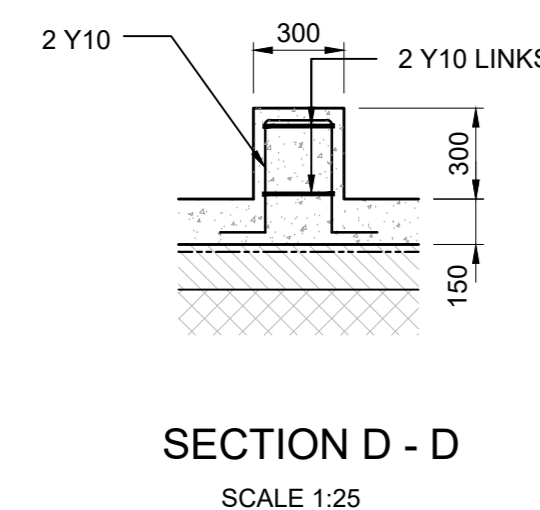
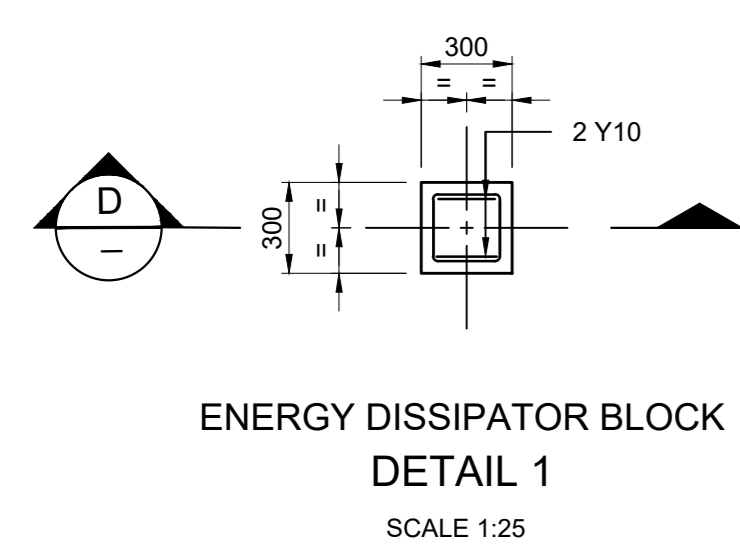
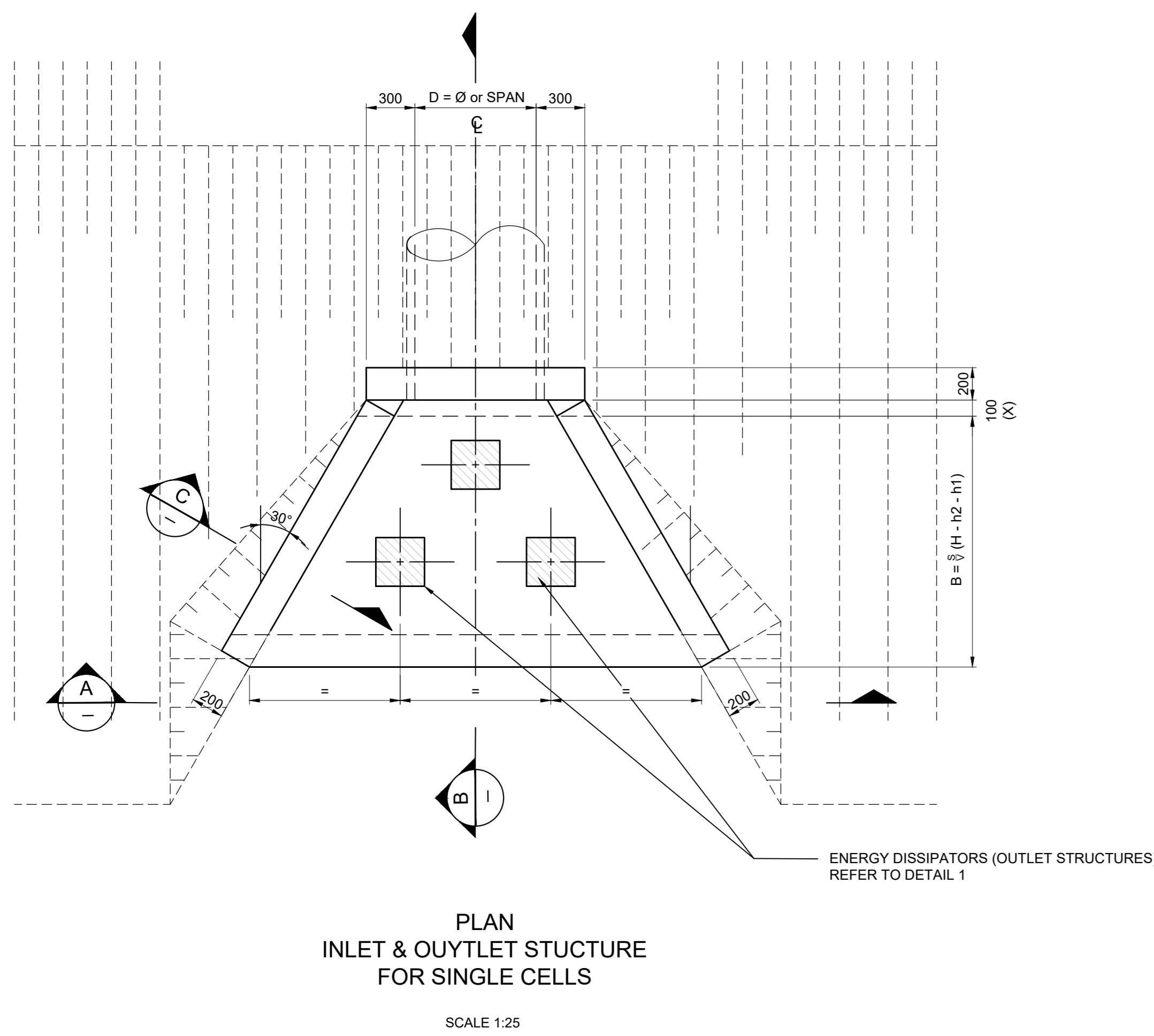
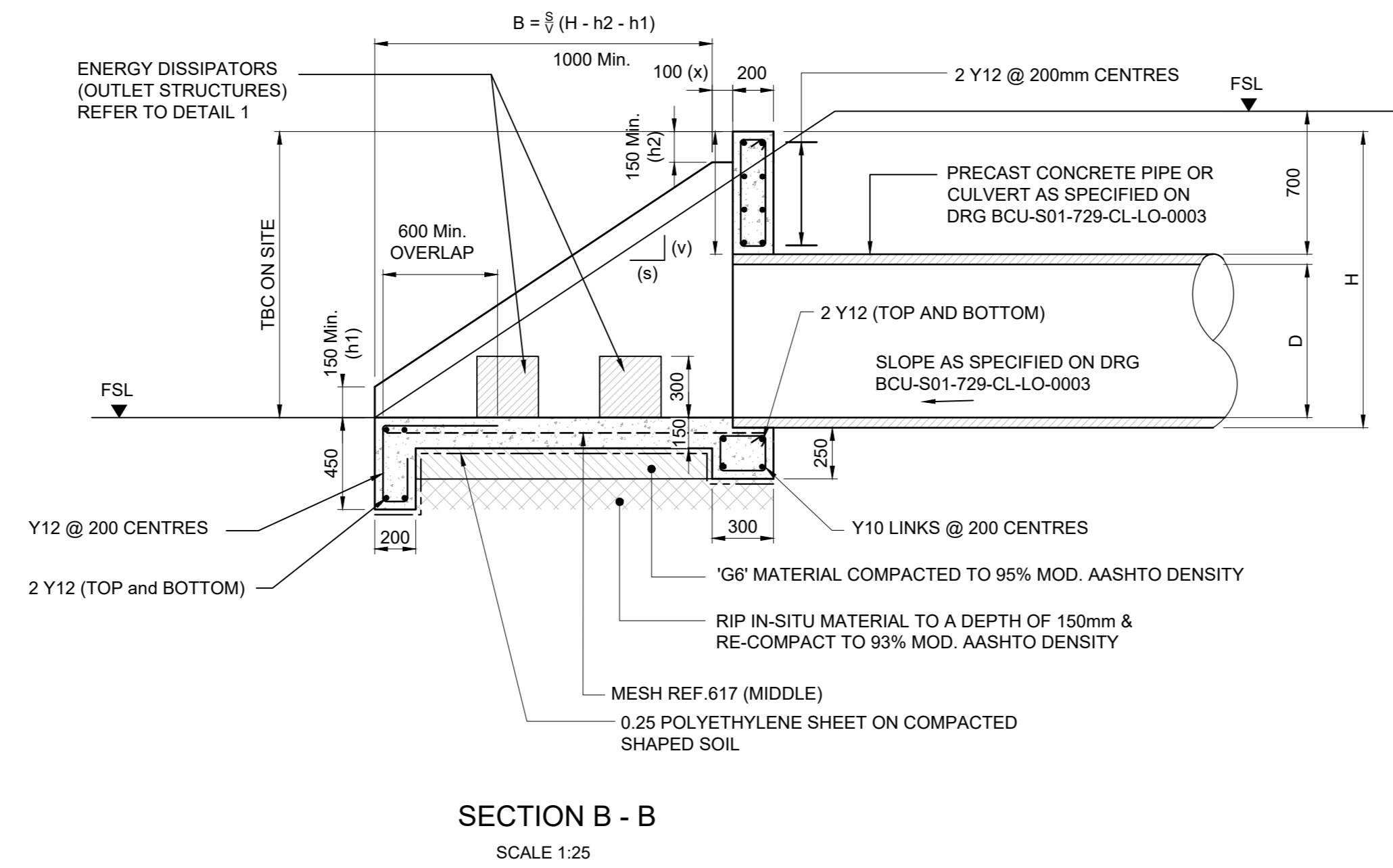
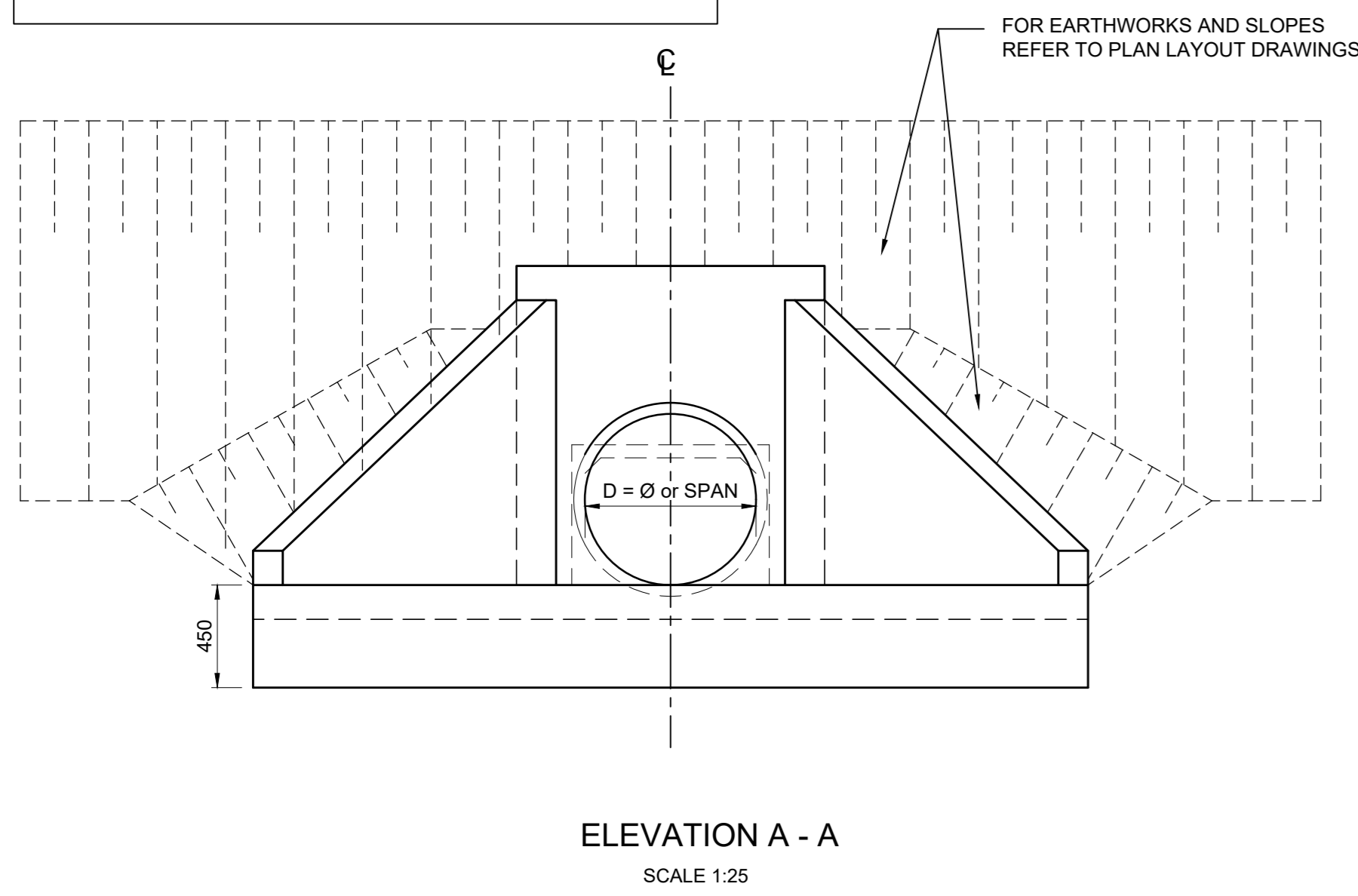
Doc #:	BCX-000017-12955-ENG-RPT-0023	<b>System Doc ID:</b>	<b>Version:</b>
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## **APPENDIX A: CIVIL INFRASTRUCTURE DRAWINGS**

<b>Doc #:</b>	BCX-000017-12955-ENG-RPT-0023	<b>System Doc ID:</b>	<b>Version:</b>
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**EROSION**  
1. EROSION PROTECTION MEASURES AS SPECIFIED BY THE ENGINEER OR AS SPECIFIED ON THE LAYOUT PLANS



**GENERAL NOTES ON CONCRETE**

- ALL DIMENSIONS IN MILLIMETERS, UNLESS OTHERWISE NOTED.
- ALL CONCRETE TO BE CLASS 35/19'S WITH A WOOD FLOAT FINISH UNLESS OTHERWISE SHOWN.
- DIMENSIONS MUST NOT BE SCALED OR ASSUMED. MISSING DIMENSIONS AND DISCREPANCIES MUST BE BROUGHT TO THE ATTENTION OF THE ENGINEER.
- DIMENSIONS AND ANCHOR BOLT LOCATIONS ARE SYMMETRICAL ABOUT CENTRE LINES UNLESS OTHERWISE NOTED.
- THE FOLLOWING TYPES OF CEMENT ARE PERMITTED FOR USE IN THE MANUFACTURE OF CONCRETE: CEM I, CEM II (S), CEM II (A/D), CEM II (A/V), CEM II (A/W) & CEM III / C. CEM III / C MAY ONLY BE USED AS A BLEND WITH CEM I. THE STRENGTH CLASS OF ALL CEMENTS USED IN THE MANUFACTURE OF CONCRETE SHALL BE 42.5N UNLESS OTHERWISE SPECIFIED ON THE DRAWING.
- CONCRETE STRENGTH IS DEFINED BY "X/Y/Z" WHERE "X" IS THE MINIMUM CUBE CRUSHING STRENGTH IN MPa AT 28 DAYS, "Y" IS THE NOMINAL MAXIMUM COARSE AGGREGATE SIZE IN mm & "Z" IS A LETTER INDICATING THE CONCRETE TYPE AS FOLLOWS:  
S = STRUCTURAL CONCRETE  
A = AGGRESSIVE ENVIRONMENT  
P = PAVING CONCRETE  
B = BLINDING CONCRETE  
WR = WATER RETAINING
- UNLESS OTHERWISE NOTED, COVER TO REINFORCEMENT IS TO BE 40mm.  
COVER IS TO BE MAINTAINED WITH THE USE OF SUITABLE SPACERS AND LIFTING BLOCKS. THE COVER BLOCKS ARE TO BE FORMED OF SAND/CEMENT MORTAR WITH A MINIMUM CEMENT : WATER RATIO OF 2.5. PATENT UNITS THAT DO NOT CORRODE MAY ALSO BE USED.
- LATERAL DIMENSIONS GIVEN ON THE DRAWINGS FOR UNDERGROUND CONCRETE ARE BASED ON CASTING AGAINST FORMWORK. WHERE UNDERGROUND CONCRETE IS TO BE CAST AGAINST EXCAVATED FACES WITHOUT FORMWORK, LATERAL DIMENSIONS OF THE CONCRETE MUST BE INCREASED TO PROVIDE A MINIMUM OF 75mm OF CONCRETE COVER AT THE EXCAVATED FACES.
- CONCRETE SURFACES SHALL BE CURED USING AN APPROVED CURING COMPOUND. (WHERE ACID PROOFING IS TO BE APPLIED TO CONCRETE SURFACE, A WAX BASED CURING COMPOUND IS NOT TO BE USED).
- UNLESS OTHERWISE NOTED, ALL 90° CORNERS OF ALL EXPOSED CONCRETE TO BE CHAMFERED 20mm x 20mm.
- BACKFILL ABOVE FOUNDATIONS AND AROUND PLINTHS TO BE IN ACCORDANCE WITH THE SPECIFICATION GIVEN IN THE GENERAL NOTES ON EARTHWORKS (ON THIS DRAWING).
- ALL GROUTING UNDER STEELWORK AND EQUIPMENT TO BE DONE BY THE CIVIL CONTRACTOR AFTER ERECTION, GENERALLY 30mm OF TO BE PROVIDED UNLESS OTHERWISE NOTED. GROUT TO BE NON-SHRINK MASTERFLOW 525 CEMENTITIOUS BEDDING GROUT BY BASF CONSTRUCTION PRODUCTS, OR SIMILAR APPROVED. TO BE APPLIED IN ACCORDANCE WITH THE MANUFACTURER'S SPECIFICATIONS.
- THE FINISH OF THE TOP SURFACE OF ALL CONCRETE IS TO BE SMOOTH FLOATED IN ACCORDANCE WITH THE PROJECT SPECIFICATION UNLESS OTHERWISE NOTED. PAVING CONCRETE IS IN ADDITION TO BE LIGHTLY BROOMED IN THE DIRECTION OF THE FALL.
- WHERE MANUFACTURER'S PRODUCTS ARE SPECIFIED, EQUIVALENT PRODUCTS MAY BE USED FROM OTHER MANUFACTURERS AFTER PRIOR WRITTEN APPROVAL OF THE ENGINEER.
- ALL BLINDING TO BE 40mm MINIMUM UNON.
- WHERE STEEL PIPES ARE CAST INTO CONCRETE, 50mm OF CONCRETE COVER IS REQUIRED TO REINFORCEMENT AND THE STEEL PIPE / PUDDLE FLANGE. THIS IS TO INSULATE THE PIPE FROM THE REINFORCEMENT AS THE PIPE MAY BE CATHODICALLY PROTECTED.
- CHUTES SHALL BE SPACED AS SPECIFIED DEPENDING ON SLOPE AND LOCALITY.
- ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH SANS 1200 & 2001, (WHICH EVER IS THE LATEST)

REFERENCE DRAWINGS			REVISIONS				
DRAWING No	DRAWING DESCRIPTION	REV	DATE	REVISION DESCRIPTION	DRN	CHK	APP
BCU-S01-729-CL-0A-0001	PLANT WTP GENERAL ARRANGEMENT	AX	15-11-2024	ISSUED FOR CLIENT REVIEW	BG	BDP	PT
BCU-S01-729-CL-0A-0001	BE AND TERRACING GENERAL ARRANGEMENT, SECTION & DETAILS	00	06-12-2024	ISSUED FOR CLIENT APPROVAL	BG	BDP	PT
BCU-S01-729-CL-0A-0001	PLANT TERRACE BLOCK PLAN						
BCU-S01-729-CL-0E-0001	WTP STORMWATER LAYOUT AND MANAGEMENT PLAN						
BCU-S01-160-CL-0A-0001	WTP ROADS LAYOUT						
BCU-S01-160-CL-0A-0001	WTP TRAFFIC AND PEDESTRIAN MANAGEMENT PLAN						

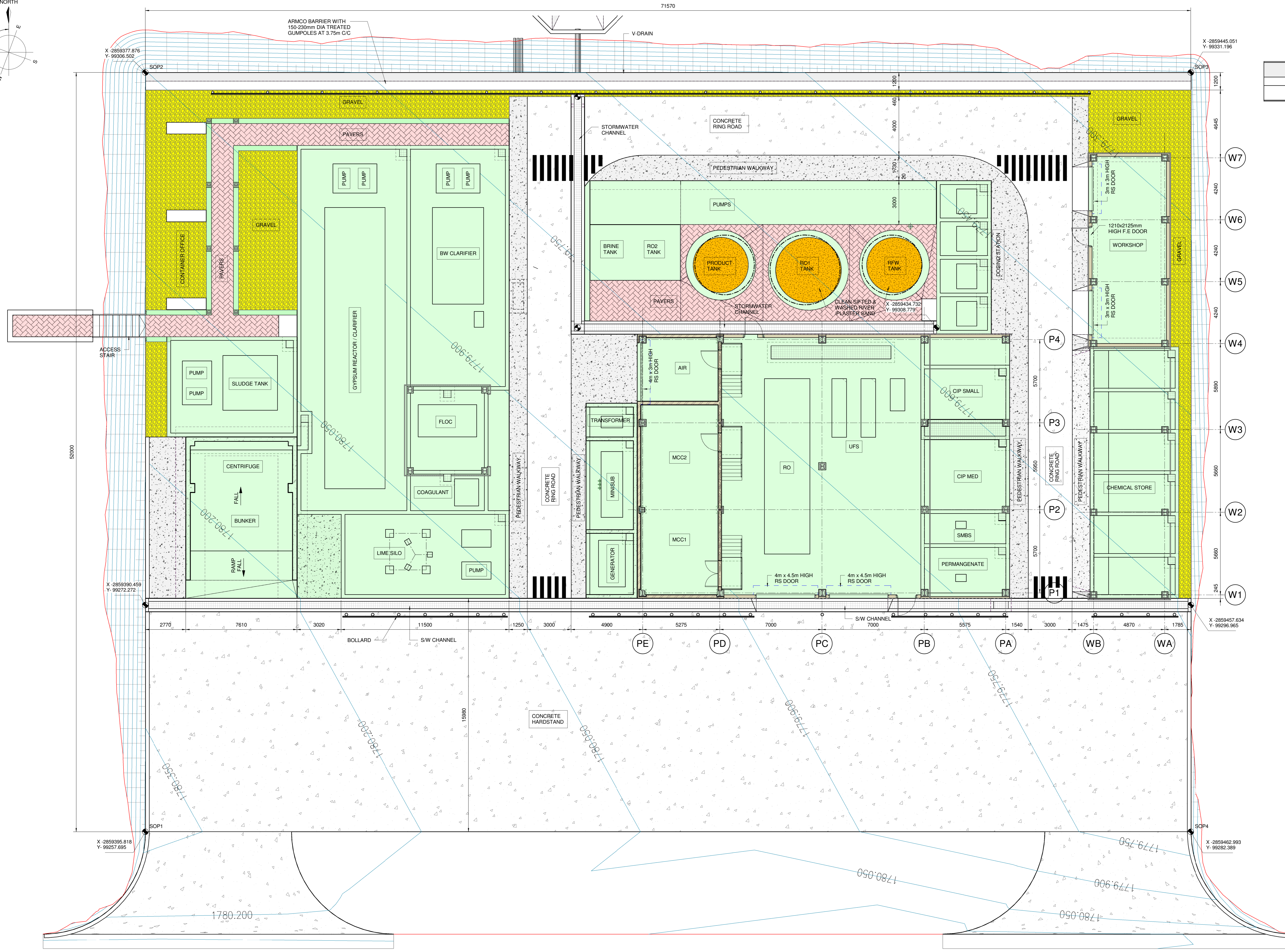
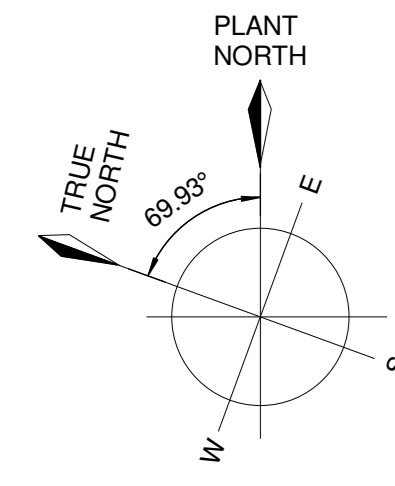
**PRIME SQUARED CONSULTING ENGINEERS**  
P.O. Box 68417, Beyersson 2021, 6 Parks Boulevard, Oxford Parks, Durban 40196, South Africa  
Telephone: (083) 450 1578, (083) 456 4342

CONSULTANT APPROVAL	
NAME	DATE
ARCHITECTURAL	15-10-2024
MECHANICAL	05-12-2024
ELECTRICAL	
CIVIL	
STRUCTURAL	
INSTRUMENTATION	
PROCESS	
ENR. MANAGER	

**exxaro**  
POWERING POSSIBILITY

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EXXARO ACCEPTANCE		CENTRE	
SIGNATURE	EMP. No.	SIGNATURE	EMP. No.
MECHANICAL		OWNERS REPRESENTATIVE	
ELECTRICAL		AREA / PROJECT MANAGER	
CIVIL		MANAGER ENGINEERING	
STRUCTURAL		PROCESS & PIPING	
ARCHITECTURAL		INSTRUMENTATION	
JOB / PROJECT NUMBER	BCX-000017	SCALE	DRAWING NUMBER
			BCU-S01-729-CL-DE-0001
		SHEET	REV
		1/1	00



**LEGEND:**

- NEW CONCRETE WORKS
- PAVERS
- GRAVEL
- CLEAN SIFTED & WASHED RIVER / PLASTER SAND
- 180mm THK PAINTED PEDESTRIAN WALKWAY
- 180mm THK CONCRETE RING ROAD & 225mm THK CONCRETE HARDSTAND
- STORMWATER CHANNEL

**CIVIL GENERAL ARRANGEMENT**  
SCALE 1 : 100

REFERENCE DRAWINGS		REVISIONS	
DRAWING No	DRAWING DESCRIPTION	REV	DATE
BCU-S01-730-CL-0001	BEW AND TERRACING	AX	15-11-2024
BCU-S01-730-CL-0002	FOUNDATION, BUNDED AREAS & SURFACE BED LAYOUT	BX	20-11-2024
		00	06-12-2024

REVISIONS		DRN	CHK	APP
REVISION DESCRIPTION	DATE			
ISSUED FOR CLIENT REVIEW	15-11-2024	GN	PT	PT
STORMWATER V-DRAIN REVISED	20-11-2024	GN	PT	PT
ISSUED FOR CLIENT APPROVAL	06-12-2024	GN	PT	PT



PR0042

CONSULTANT APPROVAL	
NAME	DATE
ARCHITECTURE	22/10/2024
MECHANICAL	05/12/2024
ELECTRICAL	
CIVIL	
STRUCTURAL	
INSTRUMENTATION	
PROCESS	
ENG. MANAGER	



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EXXARO ACCEPTANCE		EMP. No.
SIGNATURE	OWNERS REPRESENTATIVE	
MECHANICAL		
ELECTRICAL		
CIVIL		
STRUCTURAL		
ARCHITECTURAL		
PROCESS		
ING. MANAGER		

CENTRE		EMP. No.
EXXARO BELFAST COAL MINE		
BELFAST WATER TREATMENT SOLUTION		
WATER TREATMENT PLANT - INFRASTRUCTURE		
WATER TREATMENT PLANT AREA		
WATER TREATMENT AREA CIVIL		
GENERAL ARRANGEMENT		
SCALE	DRAWING NUMBER	SHEET REV
AS SHOWN	BCU-S01-730-EL-GA-0002	1 / 1 00 A0

## **APPENDIX B: STORMWATER CALCULATIONS**

<b>Doc #:</b>	BCX-000017-12955-ENG-RPT-0023	<b>System Doc ID:</b>	<b>Version:</b>
<b>TEM #:</b>	EWPM-PMG-TEM-0023	RPP2FHZ245W5-1051463680-781	<b>Revision: 01</b>

JOB NAME Proxa - Belfast WTP BFS  
 STRUCTURE Civil Infrastructure  
 TITLE Stormwater volumes  
 CALC. NO. PR0042-10-I-CAL-002

JOB NO. PR0042  
 DATE 2024/11/27  
 REVISION 001  
 CALC. BY B. du Plessis



AREA 2			15 min minimum	15			
			1:20 years peak flow				
				Exxaro standards			
		Rainfall from Exxaro	157,7				
<b>POST DEVELOPMENT RUN OFF CALCULATIONS</b>							
Surface Description	Unit	Amount	Area (m <sup>2</sup> )	C	Ft	A*C*Ft	Peak Flow (1:20)(m <sup>3</sup> /sec)
developed Land	m <sup>2</sup>	700	700,00	0,9	0,67	422,10	0,018
<b>TOTAL</b>			<b>700,00</b>			<b>Qri(pre)</b>	<b>0,018</b>

RECTANGULAR DRAIN CALC

EXXARO : WTP  
 AREA : Platform area  
 DATE : 2024/11/27

SLOPE 1:	100		
m <sup>3</sup> /s	0,018	m <sup>3</sup> /hr	66,57
B - width	0,5		
n - mannings	0,014		

Y - depth 0,4

Peak flow

average flow velocity through concrete = 4,5 - 6,0

	Area	B x Y	0,2	
	P	B + 2Y	1,3	
	R	(A/P)	0,154	
	Mannings	Q = 1/nxR^(2/3)AS^(.5)		
	0,018	(=)	0,410	Right should equal/bigger left (Not less)
	5	V = Q / A	2,05	m/s

JOB NAME Proxa - Belfast WTP BFS  
 STRUCTURE Civil Infrastructure  
 TITLE Stormwater volumes  
 CALC. NO. PR0042-10-I-CAL-002

JOB NO. PR0042  
 DATE 2024/11/27  
 REVISION 001  
 CALC. BY B. du Plessis



AREA 3			15 min minimum	15			
			1:20 years peak flow				
				Exxaro standards			
		Rainfall from Exxaro	157,7				
<b>RUN OFF CALCULATIONS</b>							
Surface Description	Unit	Amount	Area (m <sup>2</sup> )	C	Ft	A*C*Ft	Peak Flow (1:20)(m <sup>3</sup> /sec)
developed Land	m <sup>2</sup>	950	950,00	0,9	0,67	572,85	0,025
<b>TOTAL</b>			<b>950,00</b>			<b>Qri(pre)</b>	<b>0,025</b>

V - DRAIN CALC

EXXARO : WTP  
 AREA : Platform area  
 DATE : 2024/11/27

SLOPE 1:	100		
m <sup>3</sup> /s	0,025	m <sup>3</sup> /hr	90,34
n - mannings	0,014		
z - 1 :	2		
Y - depth	0,3		

Peak flow

	Area	zy <sup>2</sup> =	0,18
	P	2y √ 1+z <sup>2</sup>	1,34
	R	(A/P) =	0,134
	Mannings	Q = 1/nxR <sup>(2/3)</sup> S <sup>(.5)</sup>	
	0,025	(=)	0,34
			Right should equal left (Not less)
	V = Q / A		1,87 m/s

average flow velocity through concrete = 4,5 - 6,0